



# 2.2nV/\(\overline{Hz}\), Low-Power, 36V, OPERATIONAL AMPLIFIER

Check for Samples: OPA209, OPA2209, OPA4209

#### **FEATURES**

- LOW VOLTAGE NOISE: 2.2nV/√Hz at 1kHz
- 0.1Hz to 10Hz NOISE: 130nV<sub>PP</sub>
- LOW QUIESCENT CURRENT: 2.5mA/Ch (max)
- LOW OFFSET VOLTAGE: 150μV (max)
- GAIN BANDWIDTH PRODUCT: 18MHz
- SLEW RATE: 6.4V/μs
- WIDE SUPPLY RANGE: ±2.25V to ±18V, +4.5V to +36V
- RAIL-TO-RAIL OUTPUT
- SHORT-CIRCUIT CURRENT: ±65mA
- AVAILABLE IN SOT23-5, MSOP-8, SO-8, AND TSSOP-14 PACKAGES

#### **APPLICATIONS**

- PLL LOOP FILTERS
- LOW-NOISE, LOW-POWER SIGNAL PROCESSING
- LOW-NOISE INSTRUMENTATION AMPLIFIERS
- HIGH-PERFORMANCE ADC DRIVERS
- HIGH-PERFORMANCE DAC OUTPUT AMPLIFIERS
- ACTIVE FILTERS
- ULTRASOUND AMPLIFIERS
- PROFESSIONAL AUDIO PREAMPLIFIERS
- LOW-NOISE FREQUENCY SYNTHESIZERS
- INFRARED DETECTOR AMPLIFIERS
- HYDROPHONE AMPLIFIERS

#### **DESCRIPTION**

The OPA209 series of precision operational amplifiers achieve very low voltage noise density (2.2nV/\(\sqrt{Hz}\)) with a supply current of only 2.5mA (max). This series also offers rail-to-rail output swing, which helps to maximize dynamic range.

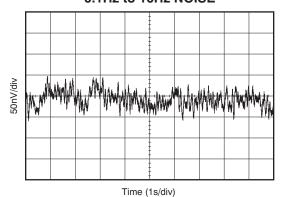
In precision data acquisition applications, the OPA209 provides fast settling time to 16-bit accuracy, even for 10V output swings. This excellent ac performance, combined with only  $150\mu V$  (max) of offset and low drift over temperature, makes the OPA209 very suitable for fast, high-precision applications.

The OPA209 is specified over a wide dual power-supply range of ±2.25 to ±18V, or single-supply operation from +4.5V to +36V.

The OPA209 is available in the SOT23-5, MSOP-8 and the standard SO-8 packages. The dual OPA2209 comes in both MSOP-8 and SO-8 packages. The quad OPA4209 is available in the TSSOP-14 package.

The OPA209 series is specified from -40°C to +125°C.

#### 0.1Hz to 10Hz NOISE



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### ORDERING INFORMATION(1)

PRODUCT	PACKAGE-LEAD	PACKAGE DESIGNATOR	PACKAGE MARKING
	SOT23-5	DBV	OOBQ
OPA209	MSOP-8	DGK	OOAQ
	SO-8	D	OPA209A
OD42200	MSOP-8	DGK	OOJI
OPA2209	SO-8	D	O2209
OPA4209	TSSOP-14	PW	OPA4209

<sup>(1)</sup> For the most current package and ordering information see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.

#### **ABSOLUTE MAXIMUM RATINGS**(1)

		OPA209, OPA2209, OPA4209	UNIT	
Supply Voltage	$V_S = (V+) - (V-)$	40	V	
Signal Input Terminal, Voltage	ge <sup>(2)</sup>	(V-) - 0.5 to (V+) + 0.5	V	
Signal Input Terminal, Curre	nt (except power-supply pins)(2)	10	mA	
Output Short-Circuit (3)		Continuous		
Operating Temperature	T <sub>A</sub>	-55 to +150	°C	
Storage Temperature	T <sub>A</sub>	-65 to +150	°C	
Junction Temperature	nction Temperature T <sub>J</sub> +2			
CCD Datings:	Human Body Model (HBM)	3000	V	
ESD Ratings:	Charged Device Model (CDM)	1000	V	

<sup>(1)</sup> Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied.

For input voltages beyond the power-supply rails, voltage or current must be limited.

<sup>(3)</sup> Short-circuit to ground, one amplifier per package.



## ELECTRICAL CHARACTERISTICS: V<sub>s</sub> = ±2.25V to ±18V

**Boldface** limits apply over the specified temperature range,  $T_A = -40^{\circ}C$  to +125°C. At  $T_A = +25^{\circ}C$ ,  $R_L = 10k\Omega$  connected to midsupply, and  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

PARAMETER			OPA209	, OPA2209, 0	DPA4209	
		CONDITIONS	MIN	TYP	MAX	UNIT
OFFSET VOLTAGE						
Input Offset Voltage	os/	$V_S = \pm 15, \ V_{CM} = 0V$		±35	±150	μV
Drift dV <sub>OS</sub> /	dΤ			1	3	μ <b>۷/°C</b>
vs Power Supply PSI	RR	$V_S = \pm 2.25 V \text{ to } \pm 18 V$		0.05	0.5	μV/V
over Temperature		V <sub>S</sub> = ±2.25V to ±18V			1	μ <b>V/V</b>
Channel Separation, dc (dual and quad versions)				1		μV/V
INPUT BIAS CURRENT						
Input Bias Current	$I_{B}$	$V_{CM} = 0V$		±1	±4.5	nA
over Temperature, -40°C to +85°C		$V_{CM} = 0V$			±8	nA
over Temperature, -40°C to +125°C		V <sub>CM</sub> = 0V			±15	nA
Input Offset Current	los	$V_{CM} = 0V$		±0.7	±4.5	nA
over Temperature, -40°C to +85°C		$V_{CM} = 0V$			±8	nA
over Temperature, -40°C to +125°C		V <sub>CM</sub> = 0V			±15	nA
NOISE						
Input Voltage Noise, = 0.1Hz to 10Hz	e <sub>n</sub>			0.13		$\mu V_{PP}$
Noise Density, f = 10Hz				3.3		nV/√ <del>Hz</del>
Noise Density, f = 100Hz				2.25		nV/√ <del>Hz</del>
Noise Density, f = 1kHz				2.2		nV/√ <del>Hz</del>
Input Current Noise Density, f = 1kHz	In			500		fA/√ <del>Hz</del>
INPUT VOLTAGE RANGE						
Common-Mode Voltage Range	′см		(V-) + 1.5V		(V+) - 1.5V	V
Common-Mode Rejection Ratio, over Temperature	RR	(V-) + 1.5V < V <sub>CM</sub> < (V+) - 1.5V	120	130		dB
INPUT IMPEDANCE						
Differential				200    4		kΩ    pF
Common-Mode				10 <sup>9</sup>    2		Ω    pF
OPEN-LOOP GAIN						
Open-Loop Voltage Gain	A <sub>OL</sub>	$(V-) + 0.2V < V_O < (V+) - 0.2V, R_L = 10k\Omega$	126	132		dB
over Temperature		$(V-) + 0.2V < V_O < (V+) - 0.2V, R_L = 10k\Omega$	120			dB
		$(V-) + 0.6V < V_O < (V+) - 0.6V, R_L = 600\Omega^{(1)}$	114	120		dB
over Temperature		$(V-) + 0.6V < V_0 < (V+) - 0.6V, R_L = 1k\Omega$	110			dB
FREQUENCY RESPONSE						
Gain Bandwidth Product GE	3W			18		MHz
Slew Rate	SR			6.4		V/μs
Phase margin	θm	$R_L = 10k\Omega$ , $C_L = 25pF$		80		Degrees
Settling Time, 0.1%	ts	G = -1, 10V Step, C <sub>L</sub> = 100pF		2.1		μS
Settling Time, 0.0015% (16-bit)		G = -1, 10V Step, C <sub>L</sub> = 100pF		2.6		μS
Overload Recovery Time		G = -1		< 1		μS
Total Harmonic Distortion + Noise THD	+N	$G = +1$ , $f = 1kHz$ , $V_O = 20V_{PP}$ , $600\Omega$		0.000025		%

<sup>(1)</sup> See the Thermal Information table for additional information.



## ELECTRICAL CHARACTERISTICS: V<sub>s</sub> = ±2.25V to ±18V (continued)

Boldface limits apply over the specified temperature range,  $T_A = -40^{\circ}$ C to +125°C.

At  $T_A = +25$ °C,  $R_L = 10$ k $\Omega$  connected to midsupply, and  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

			OPA209	, OPA2209,	OPA4209		
PARAMETER		CONDITIONS	MIN	MIN TYP		UNIT	
OUTPUT							
Voltage Output Swing		$R_L = 10k\Omega, A_{OL} > 130dB$	(V-) + 0.2V		(V+) - 0.2V	V	
		$R_L = 600\Omega$ , $A_{OL} > 114dB$	(V-) + 0.6V		(V+) - 0.6V	V	
over Temperature		$R_L = 10k\Omega$ , $A_{OL} > 120dB$	(V-) + 0.2V		(V+) - 0.2V	V	
Short-Circuit Current	I <sub>SC</sub>	$V_S = \pm 18V$		±65		mA	
Capacitive Load Drive (stable operation)	$C_{LOAD}$		See Typical Characteristics				
Open-Loop Output Impedance	Zo		See Typical Characteristics				
POWER SUPPLY							
Specified Voltage	Vs		±2.25		±18	V	
Quiescent Current (per amplifier)	ΙQ	$I_O = 0A$		2.2	2.5	mA	
over Temperature					3.25	mA	
TEMPERATURE RANGE							
Specified Range	T <sub>A</sub>		-40		+125	°C	
Operating Range	T <sub>A</sub>		<b>–</b> 55		+150	°C	

#### THERMAL INFORMATION

		OPA209AID	OPA209AIDBV	OPA209AIDGK	
	THERMAL METRIC <sup>(1)</sup>	D	DBV	DGK	UNITS
		8	5	8	
$\theta_{JA}$	Junction-to-ambient thermal resistance <sup>(2)</sup>	135.5	204.9	142.6	
JCtop	Junction-to-case (top) thermal resistance	73.7	200	46.9	
ЭЈВ	Junction-to-board thermal resistance	61.9	113.1	63.5	00044
₽JT	Junction-to-top characterization parameter	19.7	38.2	5.3	°C/W
√ <sub>JB</sub>	Junction-to-board characterization parameter	54.8	104.9	62.8	
JCbot	Junction-to-case (bottom) thermal resistance	n/a	n/a	n/a	

<sup>(1)</sup> For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.

#### THERMAL INFORMATION

		OPA2209AID	OPA2209AIDGK	OPA4209AIPW	
	THERMAL METRIC <sup>(1)</sup>	D	DGK	PW	UNITS
		8	8	14	
$\theta_{JA}$	Junction-to-ambient thermal resistance <sup>(2)</sup>	134.3	132.7	112.9	
$\theta_{JCtop}$	Junction-to-case (top) thermal resistance	72.1	38.5	26.1	
$\theta_{JB}$	Junction-to-board thermal resistance	60.7	52.1	61.0	00044
ΨЈТ	Junction-to-top characterization parameter	18.2	2.4	0.7	°C/W
ΨЈВ	Junction-to-board characterization parameter	53.8	52.8	59.2	
$\theta_{JCbot}$	Junction-to-case (bottom) thermal resistance	n/a	n/a	n/a	

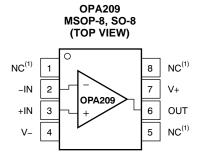
<sup>(1)</sup> For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.

<sup>(2)</sup> The junction-to-ambient thermal resistance under natural convection is obtained in a simulation on a JEDEC-standard, high-K board, as specified in JESD51-7, in an environment described in JESD51-2a.

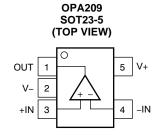
<sup>(2)</sup> The junction-to-ambient thermal resistance under natural convection is obtained in a simulation on a JEDEC-standard, high-K board, as specified in JESD51-7, in an environment described in JESD51-2a.

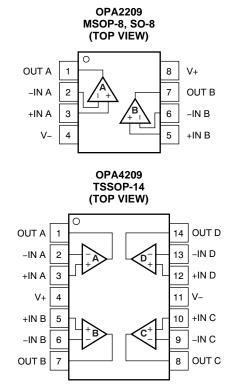


#### **PIN CONFIGURATIONS**



(1) NC = no internal connection







#### TYPICAL CHARACTERISTICS

At  $T_A = +25$ °C,  $V_S = \pm 18$ V,  $R_L = 10$ k $\Omega$  connected to midsupply, and  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

## 

Figure 1.

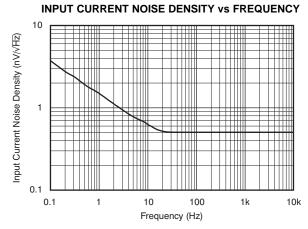


Figure 2.

#### TOTAL HARMONIC DISTORTION + NOISE RATIO vs FREQUENCY

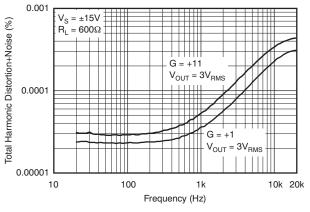


Figure 3.

#### TOTAL HARMONIC DISTORTION + NOISE RATIO vs AMPLITUDE

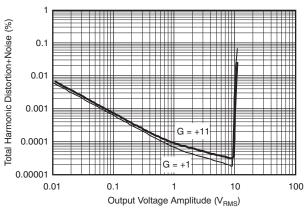


Figure 4.

## 0.1Hz TO 10Hz NOISE

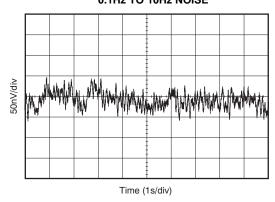


Figure 5.

# POWER-SUPPLY REJECTION RATIO vs FREQUENCY (REFERRED TO INPUT)

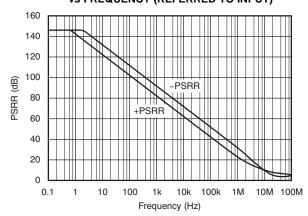
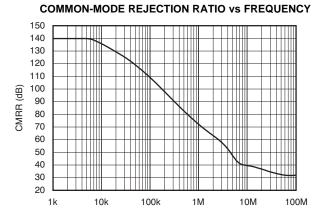


Figure 6.



At  $T_A$  = +25°C,  $V_S$  = ±18V,  $R_L$  = 10k $\Omega$  connected to midsupply, and  $V_{CM}$  =  $V_{OUT}$  = midsupply, unless otherwise noted.



Frequency (Hz)
Figure 7.

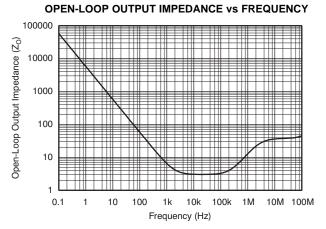


Figure 8.

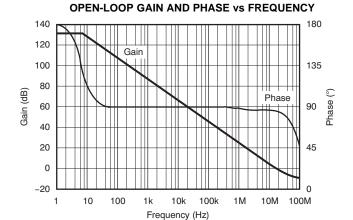


Figure 9.

**OFFSET VOLTAGE** 

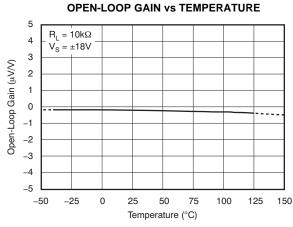
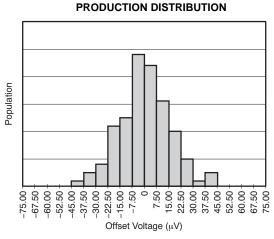


Figure 10.





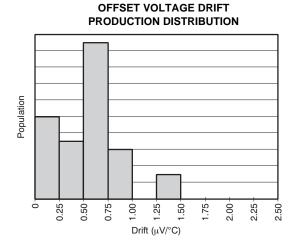


Figure 12.



At  $T_A = +25$ °C,  $V_S = \pm 18$ V,  $R_L = 10$ k $\Omega$  connected to midsupply, and  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

# INPUT BIAS AND INPUT OFFSET CURRENTS vs TEMPERATURE

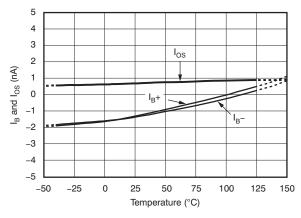


Figure 13.

#### INPUT OFFSET VOLTAGE vs COMMON-MODE VOLTAGE 100 $V_S = 36V$ 80 60 Input Offset Voltage (μV) 40 20 0 -20 -40 -60 -80 -100 (V+)-2.5V(V-)+0.5V(V-)+1.0V(V-)+1.5V(V-)+2.0V(V-)+2.5V(V+)-2.0V(V+)-1.5V(V+)-0.5VInput Common-Mode Voltage (V)

Figure 14.

#### **INPUT OFFSET VOLTAGE vs TIME**

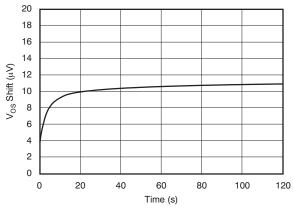


Figure 15.

#### INPUT OFFSET CURRENT vs SUPPLY VOLTAGE

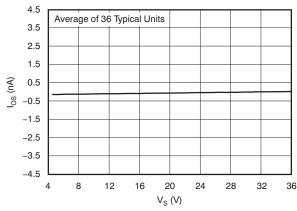


Figure 16.

#### INPUT BIAS AND INPUT OFFSET CURRENTS vs COMMON-MODE VOLTAGE

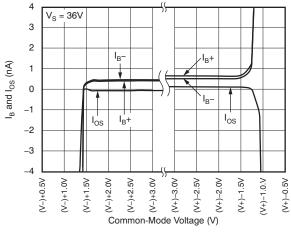


Figure 17.

#### **INPUT BIAS CURRENT vs SUPPLY VOLTAGE**

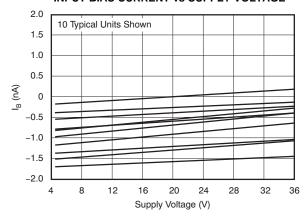
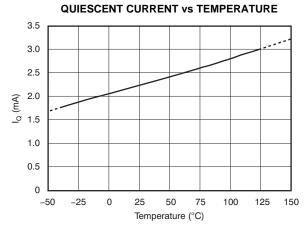


Figure 18.



At  $T_A = +25$ °C,  $V_S = \pm 18$ V,  $R_L = 10$ k $\Omega$  connected to midsupply, and  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.





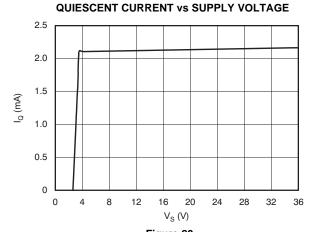


Figure 20.



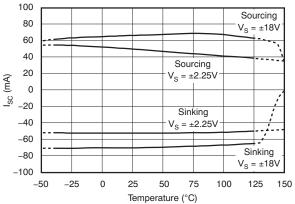


Figure 21.

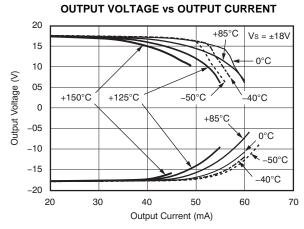


Figure 22.

## SMALL-SIGNAL STEP RESPONSE

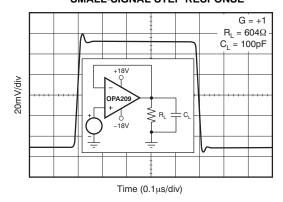


Figure 23.

#### **SMALL-SIGNAL STEP RESPONSE**

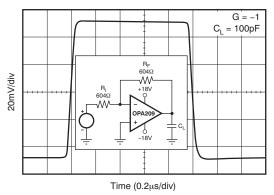


Figure 24.



At  $T_A = +25$ °C,  $V_S = \pm 18$ V,  $R_L = 10$ k $\Omega$  connected to midsupply, and  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

#### LARGE-SIGNAL STEP RESPONSE

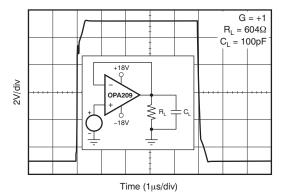


Figure 25.

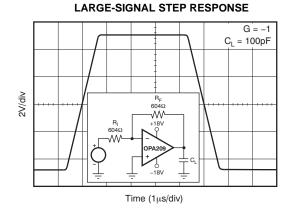


Figure 26.

#### **NO PHASE REVERSAL**

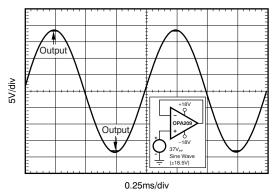
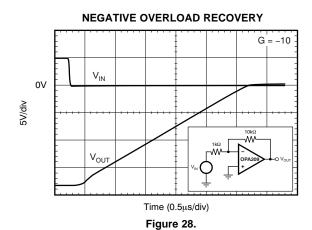


Figure 27.



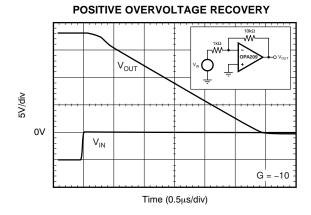


Figure 29.

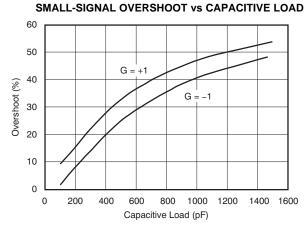


Figure 30.



#### APPLICATION INFORMATION

#### **DESCRIPTION**

The OPA209 series of precision operational amplifiers are unity-gain stable, and free from unexpected output and phase reversal. Applications with noisy or high-impedance power supplies require decoupling capacitors placed close to the device pins. In most cases,  $0.1\mu F$  capacitors are adequate. Figure 31 shows a simplified schematic of the OPA209. This die uses a SiGe bipolar process and contains 180 transistors.

#### **OPERATING VOLTAGE**

The OPA209 series of op amps can be used with single or dual supplies within an operating range of  $V_S = +4.5V$  (±2.25V) up to +36V (±18V). Supply voltages higher than 40V total can permanently damage the device; see the Absolute Maximum Ratings table.

In addition, key parameters are assured over the specified temperature range,  $T_A = -40^{\circ}\text{C}$  to +125°C. Parameters that vary significantly with operating voltage or temperature are shown in the Typical Characteristics section of this data sheet.

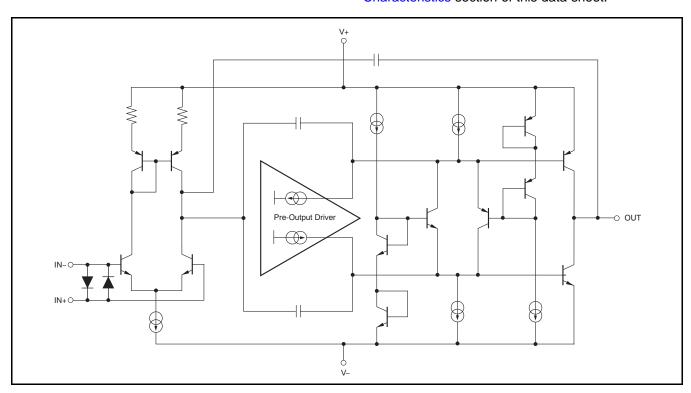


Figure 31. OPA209 Simplified Schematic

# TEXAS INSTRUMENTS

#### INPUT PROTECTION

The input terminals of the OPA209 are protected from excessive differential voltage with back-to-back diodes, as shown in Figure 32. In most circuit applications, the input protection circuitry has no consequence. However, in low-gain or G = 1 circuits, fast ramping input signals can forward-bias these diodes because the output of the amplifier cannot respond rapidly enough to the input ramp. This effect is illustrated in Figure 25 and Figure 26 of the Typical Characteristics. If the input signal is fast enough to create this forward-bias condition, the input signal current must be limited to 10mA or less. If the input signal current is not inherently limited, an input series resistor can be used to limit the signal input current. This input series resistor degrades the low-noise performance of the OPA209. See the Noise Performance section for further information on noise performance. Figure 32 shows an example configuration that implements a current-limiting feedback resistor.

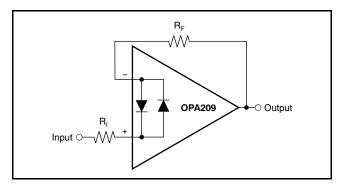


Figure 32. Pulsed Operation

#### **NOISE PERFORMANCE**

Figure 33 shows the total circuit noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). Two different op amps are shown with the total circuit noise calculated. The OPA209 has very low voltage noise, making it ideal for low source impedances (less than  $2k\Omega$ ). As a comparable precision FET-input op amp (very low current noise), the OPA827 has somewhat higher voltage noise, but lower current noise. It provides excellent noise performance at moderate to high source impedance ( $10k\Omega$  and up). For source impedance lower than  $300\Omega$ , the OPA211 may provide lower noise.

The equation in Figure 33 shows the calculation of the total circuit noise, with these parameters:

- e<sub>n</sub> = voltage noise,
- i<sub>n</sub> = current noise,
- R<sub>S</sub> = source impedance,
- k = Boltzmann's constant = 1.38 x 10<sup>-23</sup> J/K,
- and T = temperature in kelvins.

For more details on calculating noise, see the *Basic Noise Calculations* section.

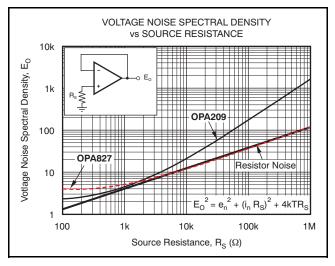


Figure 33. Noise Performance of the OPA209 and OPA827 in Unity-Gain Buffer Configuration

#### **BASIC NOISE CALCULATIONS**

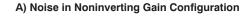
Low-noise circuit design requires careful analysis of all noise sources. External noise sources can dominate in many cases; consider the effect of source resistance on overall op amp noise performance. Total noise of the circuit is the root-sum-square combinations of all noise components.

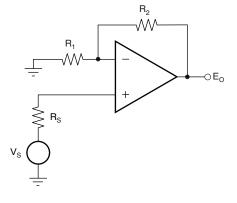
The resistive portion of the source impedance produces thermal noise proportional to the square root of the resistance. This function is illustrated in Figure 33. The source impedance is usually fixed; consequently, select the appropriate op amp and the feedback resistors to minimize the respective contributions to the total noise.



Figure 34 illustrates both noninverting (Figure 34a) and inverting (Figure 34b) op amp circuit configurations with gain. In circuit configurations with gain, the feedback network resistors also contribute noise. The current noise of the op amp reacts with the feedback resistors to create additional noise components.

The feedback resistor values can generally be chosen to make these noise sources negligible. Note that low-impedance feedback resistors load the output of the amplifier. The equations for total noise are shown for both configurations.





Noise at the output:

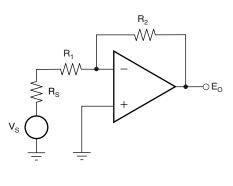
$${\mathsf E_0}^2 = \left[1 + \frac{{\mathsf R_2}}{{\mathsf R_1}}\right]^2 \, {\mathsf e_n}^2 + {\mathsf e_1}^2 + {\mathsf e_2}^2 + {(\mathsf i_n^{} \mathsf R_2)}^2 + {\mathsf e_S}^2 + {(\mathsf i_n^{} \mathsf R_S)}^2 \right] 1 + \frac{{\mathsf R_2}}{{\mathsf R_1}}$$

Where 
$$e_S = \sqrt{4kTR_S} \times \left[1 + \frac{R_2}{R_1}\right]$$
 = thermal noise of  $R_S$ 

$$e_1 = \sqrt{4kTR_1} \times \left(\frac{R_2}{R_1}\right) = \text{thermal noise of } R_1$$

$$e_2 = \sqrt{4kTR_2}$$
 = thermal noise of  $R_2$ 

#### B) Noise in Inverting Gain Configuration



Noise at the output:

$$E_{O}^{2} = \left[1 + \frac{R_{2}}{R_{1} + R_{S}}\right]^{2} e_{n}^{2} + e_{1}^{2} + e_{2}^{2} + (i_{n}R_{2})^{2} + e_{S}^{2}$$

Where 
$$e_S = \sqrt{4kTR_S} \times \left[ \frac{R_2}{R_1 + R_S} \right]$$
 = thermal noise of  $R_S$ 

$$e_1 = \sqrt{4kTR_1} \times \left[ \frac{R_2}{R_1 + R_S} \right]$$
 = thermal noise of  $R_1$ 

$$e_2 = \sqrt{4kTR_2}$$
 = thermal noise of  $R_2$ 

NOTE: For the OPA209 series op amps at 1kHz,  $e_n = 2.2 \text{nV}/\sqrt{\text{Hz}}$  and  $I_n = 530 \text{fA}/\sqrt{\text{Hz}}$ .

Figure 34. Noise Calculation in Gain Configurations



#### **ELECTRICAL OVERSTRESS**

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

It is helpful to have a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event. See Figure 35 for an illustration of the ESD circuits contained in the OPA209 series (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where they meet at an absorption device internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.

An ESD event produces a short duration, high-voltage pulse that is transformed into a short duration, high-current pulse as it discharges through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent it from being damaged. The energy absorbed by the protection circuitry is then dissipated as heat.

When an ESD voltage develops across two or more of the amplifier device pins, current flows through one or more of the steering diodes. Depending on the path that the current takes, the absorption device may activate. The absorption device has a trigger, or threshold voltage, that is above the normal operating voltage of the OPA209 but below the device breakdown voltage level. Once this threshold is exceeded, the absorption device quickly activates and clamps the voltage across the supply rails to a safe level.

When the operational amplifier connects into a circuit such as the one Figure 35 shows, the ESD protection components are intended to remain inactive and not become involved in the application circuit operation. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. Should this condition occur, there is a risk that some of the internal ESD protection circuits may be biased on, and conduct current. Any such current flow occurs through steering diode paths and rarely involves the absorption device.

Figure 35 depicts a specific example where the input voltage,  $V_{IN}$ , exceeds the positive supply voltage (+V<sub>S</sub>) by 500mV or more. Much of what happens in the circuit depends on the supply characteristics. If +V<sub>S</sub> can sink the current, one of the upper input steering diodes conducts and directs current to +V<sub>S</sub>. Excessively high current levels can flow with increasingly higher  $V_{IN}$ . As a result, the datasheet specifications recommend that applications limit the input current to 10mA.

If the supply is not capable of sinking the current,  $V_{IN}$  may begin sourcing current to the operational amplifier, and then take over as the source of positive supply voltage. The danger in this case is that the voltage can rise to levels that exceed the operational amplifier absolute maximum ratings.

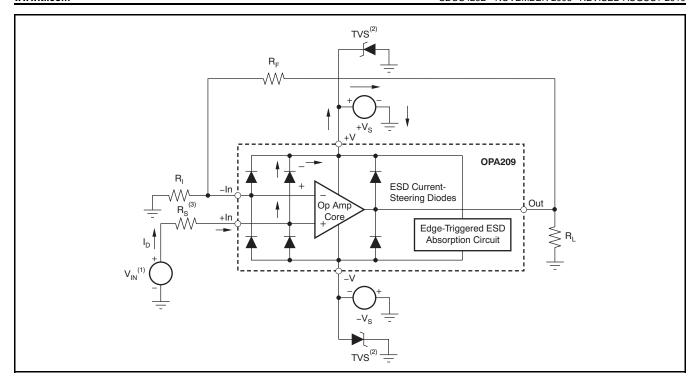
Another common question involves what happens to the amplifier if an input signal is applied to the input while the power supplies  $+V_S$  and/or  $-V_S$  are at 0V.

Again, it depends on the supply characteristic while at 0V, or at a level below the input signal amplitude. If the supplies appear as high impedance, then the operational amplifier supply current may be supplied by the input source via the current steering diodes. This state is not a normal bias condition; the amplifier most likely will not operate normally. If the supplies are low impedance, then the current through the steering diodes can become quite high. The current level depends on the ability of the input source to deliver current, and any resistance in the input path.

If there is an uncertainty about the ability of the supply to absorb this current, external zener diodes may be added to the supply pins as shown in Figure 35. The zener voltage must be selected such that the diode does not turn on during normal operation.

However, its zener voltage should be low enough so that the zener diode conducts if the supply pin begins to rise above the safe operating supply voltage level.





- (1)  $V_{IN} = +V_S + 500$ mV.
- (2) TVS:  $+V_{S(max)} > V_{TVSBR (Min)} > +V_{S}$
- (3) Suggested value approximately  $1k\Omega$ .

Figure 35. Equivalent Internal ESD Circuitry and Its Relation to a Typical Circuit Application



13-Jan-2011

#### **PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/ Ball Finish	MSL Peak Temp <sup>(3)</sup>	Samples (Requires Login)
OPA209AID	ACTIVE	SOIC	D	8	75	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Request Free Samples
OPA209AIDBVR	ACTIVE	SOT-23	DBV	5	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Request Free Samples
OPA209AIDBVT	ACTIVE	SOT-23	DBV	5	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Contact TI Distributor or Sales Office
OPA209AIDGKR	ACTIVE	MSOP	DGK	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Purchase Samples
OPA209AIDGKT	ACTIVE	MSOP	DGK	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Request Free Samples
OPA209AIDR	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Purchase Samples
OPA2209AID	ACTIVE	SOIC	D	8	75	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Contact TI Distributor or Sales Office
OPA2209AIDGKR	ACTIVE	MSOP	DGK	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Purchase Samples
OPA2209AIDGKT	ACTIVE	MSOP	DGK	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Request Free Samples
OPA2209AIDR	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Request Free Samples
OPA4209AIPW	ACTIVE	TSSOP	PW	14	90	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Request Free Samples
OPA4209AIPWR	ACTIVE	TSSOP	PW	14	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	Purchase Samples

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.



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13-Jan-2011

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Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL. Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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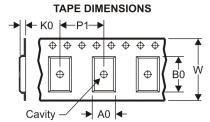
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## PACKAGE MATERIALS INFORMATION

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## TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
	Dimension designed to accommodate the component length
K	Dimension designed to accommodate the component thickness
V	/ Overall width of the carrier tape
ГР	Pitch between successive cavity centers

#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA209AIDBVR	SOT-23	DBV	5	3000	180.0	8.4	3.2	3.1	1.39	4.0	8.0	Q3
OPA209AIDBVT	SOT-23	DBV	5	250	180.0	8.4	3.2	3.1	1.39	4.0	8.0	Q3
OPA209AIDGKR	MSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA209AIDGKT	MSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA209AIDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
OPA2209AIDGKR	MSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA2209AIDGKT	MSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA2209AIDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
OPA4209AIPWR	TSSOP	PW	14	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1

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\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA209AIDBVR	SOT-23	DBV	5	3000	190.5	212.7	31.8
OPA209AIDBVT	SOT-23	DBV	5	250	190.5	212.7	31.8
OPA209AIDGKR	MSOP	DGK	8	2500	346.0	346.0	29.0
OPA209AIDGKT	MSOP	DGK	8	250	190.5	212.7	31.8
OPA209AIDR	SOIC	D	8	2500	346.0	346.0	29.0
OPA2209AIDGKR	MSOP	DGK	8	2500	346.0	346.0	29.0
OPA2209AIDGKT	MSOP	DGK	8	250	190.5	212.7	31.8
OPA2209AIDR	SOIC	D	8	2500	346.0	346.0	29.0
OPA4209AIPWR	TSSOP	PW	14	2000	346.0	346.0	29.0

# DBV (R-PDSO-G5)

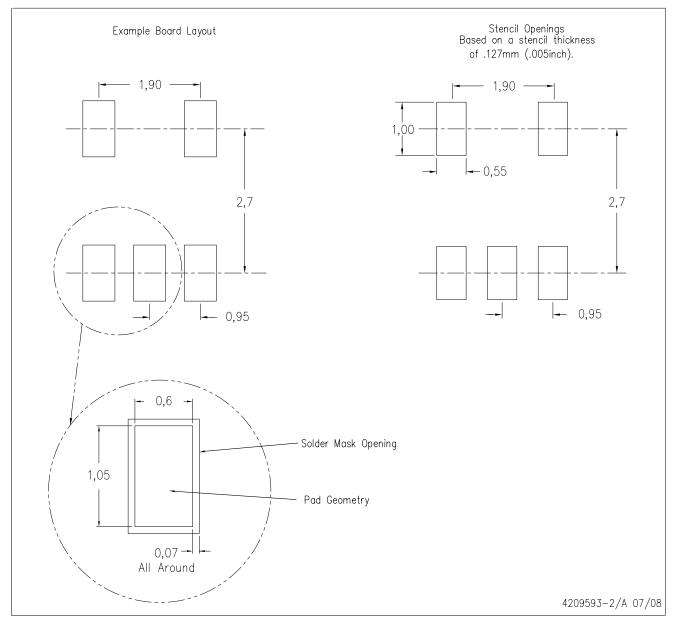
## PLASTIC SMALL-OUTLINE PACKAGE



- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
  - D. Falls within JEDEC MO-178 Variation AA.



# DBV (R-PDSO-G5)



- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.



# DGK (S-PDSO-G8)

## PLASTIC SMALL-OUTLINE PACKAGE



- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
- E. Falls within JEDEC MO-187 variation AA, except interlead flash.



PW (R-PDSO-G14)

## PLASTIC SMALL OUTLINE

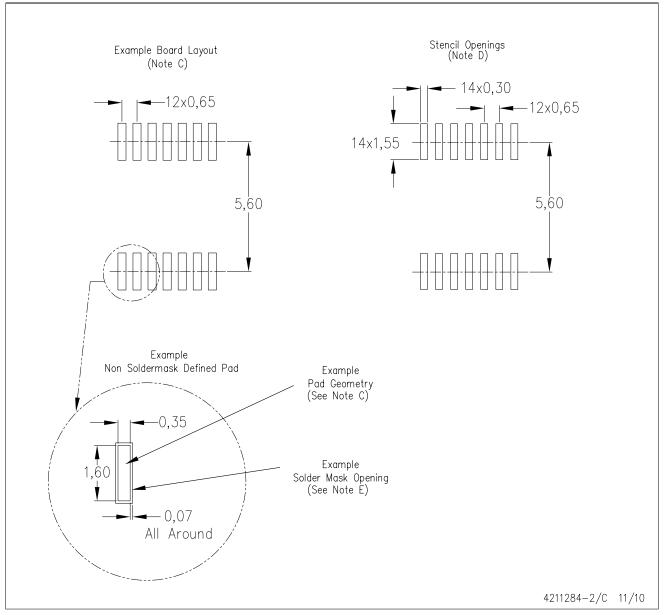


- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M—1994.
- B. This drawing is subject to change without notice.
  - Sody length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
- Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
- E. Falls within JEDEC MO-153



# PW (R-PDSO-G14)

## PLASTIC SMALL OUTLINE

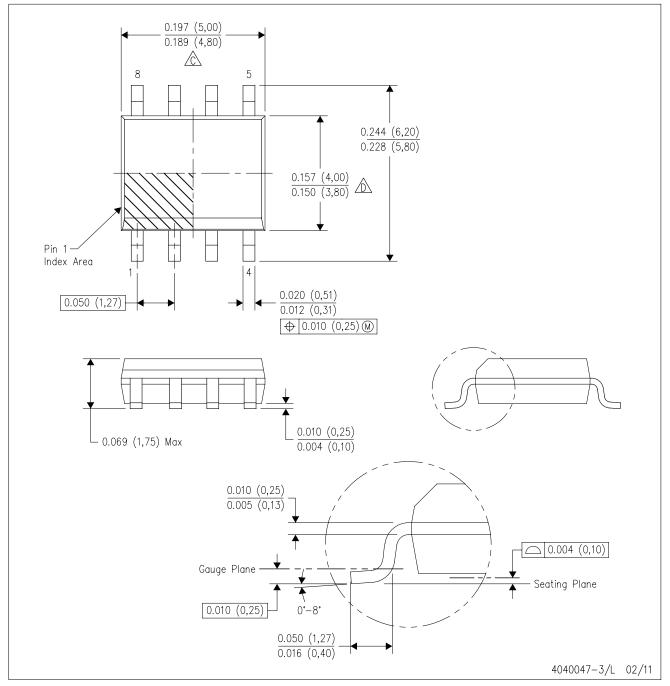


- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



## D (R-PDSO-G8)

## PLASTIC SMALL OUTLINE

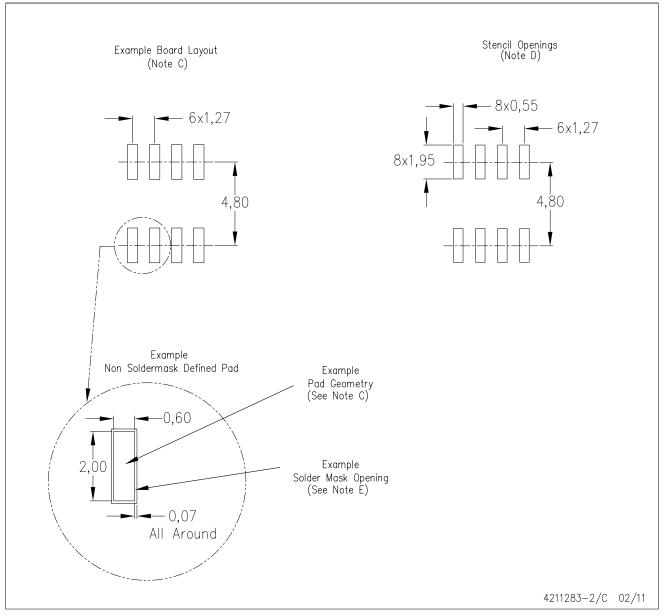


- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
- E. Reference JEDEC MS-012 variation AA.



# D (R-PDSO-G8)

## PLASTIC SMALL OUTLINE



- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



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